

Estimation of abrasion rates of regolith particles on Itokawa and the Moon based on abrasion experiments.

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External 3D shapes and surface morphologies of Itokawa and lunar regolith particles examined by X-ray nanotomography and SEM showed that some particles have rounded edges, which should be formed by mechanical abrasion [1-3]. Seismic shaking by micrometeoroid impacts on the Itokawa surface was proposed for the abrasion [1]. In order to understand abrasion processes and evolution of regolith particles on the airless bodies, abrasion experiments have been made [4,5]. In this study, we have performed additional abrasion experiments together with SEM observation of abraded grains in order to examine abrasion process and obtain a general equation for the abrasion rate and the results were applied to abrasion of Itokawa and lunar particles.

The samples used were quartz, olivine (Fo₉₀) and basalt. They were crushed and grains 1~2 mm in size were selected except for some to examine grain size effect (0.5~1 mm and 2~4 mm). These grains (~6.5g) were put into a vessel (10 mL) of agate, dunnite or basalt with ~50% fraction. Then the vessel was shaken with vertically-vibrational motion in a mill (Multi-beads-shocker: YASUIKIKAI Co.). Powder with the size less than 1/6 of the grain size (e.g., <250 μm for 1~2 mm grains) produced by abrasion was removed by sieving. The amount of abrasion, P , was defined as the difference between the grain masses before and after the abrasion, which was normalized by the initial grain mass.

For quartz grains, P increases with abrasion duration, t , (20 sec to 360 min) with the power of ~0.25 irrespective of vibration rate, Ω (100 to 2500 rpm). The amount of abrasion in the first 1 min, P_1 , increases with Ω (100 to 3000 rpm) for quartz, olivine and basalt. The powers of P_1 - Ω relation, m_i , at $\Omega < \sim 700$ rpm ($m = 0.1 \sim 0.4$) are smaller than those at $\Omega > \sim 700$ rpm ($m_i = 1.2 \sim 2$). P_1 increases with the grain size, d , at $\Omega = 2000$ rpm for quartz and the power value is temporally ~1.6. If we assume that the power relation between P and t is applicable to different sample materials and that between P_1 and d to different sample materials and Ω , we can obtain the following equation; $P = A_i \times \Omega^{m_i} \times d^{1.6} \times t^{0.25}$ (Eq.1), where A_i is the proportionality and the suffix i denote the sample materials. SEM observation together with the P - t relation showed that the abrasion advances by chipping grain corners (chipping) for $P < \sim 1\%$ while grain corners and edges become rounded (wearing) for $P > \sim 1\%$.

The maximum accelerations by impact on Itokawa and the Moon can be estimated to be ~1 and ~100 m/s² based on the impact experiments [6], which correspond to Ω of ~100 and ~700 rpm, respectively. This gives A_i 's in Eq.1 with $d = 1.5$ mm and $t = 1$ min are ~0.2 % (olivine) on Itokawa and ~0.5 % (basalt) on the Moon. If typical grain convection time by impact of ~180 s on Itokawa [7] is adopted as the maximum value of t , P is estimated to be ~0.003 and ~0.1 % for $d = 100$ μm and 1 mm, respectively. As the Itokawa grains have rounded edges (wearing), $> 4 \times 10^9$ and > 3000 times of impact are required, respectively, for $P > 1\%$. If the impact frequency on Itokawa [7] is considered, these numbers of impact required for wearing are too large, suggesting that grain abrasion on Itokawa is not expected and impact on the larger parent body ($> \sim 20$ km) [8] should be necessary. In contrast, on the Moon, $A_i \sim 0.5\%$ suggests possible abrasion because of longer residence time in a regolith layer than Itokawa.

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