ラマン増幅器用シリコングレーティング導波路の設計 Design of Silicon Grating Waveguides for Raman Amplifier 東大生研、[○]蕭 逸華、岩本 敏、荒川 泰彦 IIS, Univ. of Tokyo, [°]Yi-Hua Hsiao, Satoshi Iwamoto, and Yasuhiko Arakawa E-mail: yihua@iis.u-tokyo.ac.jp

Silicon photonics is regarded as a key technology for low cost production and on-chip integration of nanophotonic devices. To realize efficient silicon-based light sources, recently some works reported stimulated Raman scattering (SRS) in silicon photonic crystal (PhC) waveguide (WG) [1-3]. In our previous report [4], we proposed a design that support two WG modes with symmetric electric field distributions, which can be coupled from outside efficiently. Furthermore, both pump and Stokes wavelengths are designed in ultraslow-light regions. However, considering CMOS-compatible fabrication processes, simple geometry structures are strongly needed. In this report, we design silicon grating WGs (GWGs) for high gain factor (G.F.) Raman amplifier. The optimized structures not only keep the advantages that we reported before [4], but also have simple structure for easier fabrication.

The figure of merit is estimated by calculating a $G.F. \equiv S_s S_p / A_R$, where S_s and S_p are slow down factors (*S*, defined as $n_g / n_{si} = c/n_{si}v_g$, *c* is light velocity in vacuum, n_g is group index, and n_{si} is refractive index of silicon) of Stokes and pump signal, respectively. A_R is Raman cross section effective area defined in Ref.[3].

The basic structure in our study is a mechanically strong silicon grating WGs with SiO₂ cladding in the vertical and in-plane directions as shown in Fig. 1 (a). The thickness of the slab is 0.48*a* (*a* is the period of grating). As Fig. 1 (b), the grating shape could be controlled by changing the parameters *x* and *y* of grating fins. We firstly investigate the band structure of TE-like modes with *x* of 0.2 and *y* of 0.64 as shown in Fig. 1 (c). There are three modes named A, B, and C in the low order modes region. The mode A (Fig. 1 (d)) and B (Fig. 1 (e)) are symmetric modes, and mode C (Fig. 1 (f)) is anti-symmetric mode. As symmetric modes could be coupled from outside efficiency, the mode A and B could be set as Stokes frequency and pump frequency respectively. In order to match the Raman shift of silicon $\Delta \omega_R = 2\pi \times 15.6$ THz, the frequencies of mode A and B are calculated by fixing *x*=0.2 and tuning *y* as shown in Fig. 1 (g). The frequency difference $\omega_B \cdot \omega_A$ and the corresponding $\Delta \omega_R$ as we set pump wavelength as 1.55µm are also calculated in Fig. 1 (g). The cross point of two lines mean that the frequency difference at the Brillouin edge matches the Raman shift of silicon as *y* of 0.64 and *a* of 0.439 µm.

 v_g , A_R , and *G.F.* of is summarized in Table I with the best result in the past works [2] and our previous report [4]. Our new design shows good performance in *G.F.* along crystal direction [110], which is 92 times as large as previous works from other groups. This enhancement is attributed to the smaller A_R and ultra-low v_g for pump and Stokes modes. Furthermore, slow pump mode is accessible from outside because only symmetric modes are used. Importantly, the *G.F.* of GWG is the same order as our previous work [4], and the simple shape structures could easily fabricate by CMOS-compatible processes. Therefore, our designs are directly applicable to Silicon Raman amplifiers and lasers.

	Table I Performance comparison in different scheme				
Туре	$v_{g,p}$	$v_{\rm g,s}$	Along	$A_{\rm R}(\mu {\rm m}^2)$	$G.F.~(\mu m^{-2})$
Ref[3]	$2.18 \times 10^{-1}c$	$1.70 \times 10^{-4}c$	[100]	0.4185	5.37×10^{3}
			[110]	0.4142	5.43×10^{3}
Ref[4]	$1.23 \times 10^{-4}c$	$2.37 \times 10^{-3}c$	[100]	0.7678	3.72×10^{5}
			[110]	0.4424	6.46×10^5
GWG	$7.79 \times 10^{-4} c$	$6.80 \times 10^{-4} c$	[100]	0.3426	4.59×10^{5}
			[110]	0.3148	5.00×10^{5}

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Fig. 1 (a)-(b) Illustration of grating WG, where x and y define the grating shape. (c) Band structures of x=0.2, y=0.64 calculated by plane-wave-expansion method. The E_y mode profile of (d) mode A, (e) mode B, and (f) mode C. (g) The frequencies and the frequency difference of mode A and B by tuning y, and the $\Delta\omega_R$ when we set the wavelength of mode B as 1.55µm.