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A-3-6 A HIGH CURRENT GAIN, HIGH SPEED POWER GATE ASSOCIATED TRANSISTOR

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It has been desired to develop power transistors with common-emitter current gain  $(h_{FE})$  of more than 20 and both rise time  $(t_r)$  and fall time  $(t_f)$  of less than 0.2µs for application to high speed inverters operating at 50 - 100 kHz.

Unfortunately, transistors have inherent difficulties for achieveing high current gain, high switching speed and high collector voltage simultaneously. So that conventional power transistors have  $h_{\rm FE}$  of less than 10, both  $t_{\rm r}$  and  $t_{\rm f}$  of more than 0.3µs, collector-emitter sustaining voltage ( $V_{\rm CER}(sus)$ ) of 650 V and average collector current rating ( $I_{\rm AC}$ ) of 50 A.

Gate Associated Transistors (GAT's), proposed by us,  $^{1)-4}$  have been shown to overcome above difficulties. However, high power GAT with a current rating of 50A needs further development to satisfy above requirement.

We developed here a multi-emitter GAT. Optimum design of gate structure and multi-emitter structure decreased capacitance between gate and emitter and also reduced fall-off of current gain at high collector current.

In this paper, characteristics of the power GAT are described. The GAT has  $h_{FE}$  of 30,  $t_r$  of 0.17µs,  $t_f$  of 0.15µs,  $V_{CER(sus)}$  of 630 V and  $I_{AC}$  of 50 A. The  $h_{FE}$  of the GAT is about 5 times as high as that of the conventional power transistor and both the  $t_r$  and the  $t_f$  of the former is about one half of those of the latter.

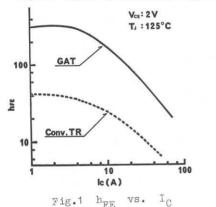
Fig.1 shows typical measurements of  $h_{\rm FE}$  vs. collector current of both the GAT and the conventional power transistor. High  $h_{\rm FE}$  in the GAT is achieved by the gate shielding effect<sup>1</sup>) and the relatively small fall-off in the  $h_{\rm FE}$  at high collector current is accomplished by means of the multi-emitter structure. Fig.2 shows typical measurements of collector-emitter saturation voltage ( $V_{\rm CE}({\rm sat})$ ) vs. base current ( $I_{\rm B}$ ) of both transistors. The  $I_{\rm B}$  of the conventional transistor is about 3 times as large as that of the GAT at which  $V_{\rm CE}({\rm sat})$ 's of both transistors are same. This implys that a base circuit for the GAT can be simple compared with that of the conventional transistor. Fig.3 shows a turn-on wave form of collector current in the GAT. The  $t_{\rm r}$  of the GAT is 0.17 µs when  $I_{\rm B}$ =4A, while that of the conventional transistor is 0.50 µs when  $T_{\rm B}$ =10A. The transistor is 0.49 V when  $I_{\rm B}$ =10A. These results imply that both a transient loss and a steady state loss of the GAT is smaller than those of the conventional transistor, moreover

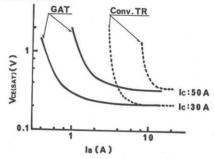
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that the base current of the former can be loss than one half of that of the latter. Table I shows electrical characteristics of the GAT compared with those of the conventional transistor.

In conclusion, application of the power GAT is suitable for improving performance of high power switching circuits because it shows smaller switching loss and it needs lower base current than the conventional transistor. The power GAT is promising for application to high speed inverters operating at 50 - 100 kHz.

Ackowledgements: The authors with to thank Dr. K.Shirahata for his encouragement. References: 1)H.Kondo,et al.,IEEE Trans.Electron Devices,vol.ED-27,pp.373-379,1980. 2)H.Kondo,et al.,1979 IEEE ISSCC Dig.Tech.Papers,vol.22,p.84. 3)H.Kondo,et al., 1979 International Conf.on Solid State Devices,Tokyo,A-6-13. 4)H.Kondo,et al., Japan.J.Appl.Phys.,vol.18,Supp.18-1,pp.329-333,1979.







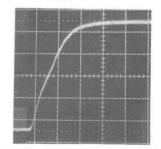


Table I Electrical characterictics of power GAT and conventional transistor

Fig.3

Turn-on wave form of the collector

I<sub>B</sub>=4A,I<sub>C</sub>=50A,V<sub>CC</sub>=300V V:10A/div. H:0.1µs/div.

current of the power GAT

|                            | Power GAT |  | Conventional transistor |   |
|----------------------------|-----------|--|-------------------------|---|
| BV <sub>CBO</sub> (V)      | 680       | I <sub>CBO</sub> =150µА  | 690                     | I <sub>CB0</sub> =150µл   |
| BV <sub>CER(sus)</sub> (V) | 630       | $I_{C}=1\Lambda, R_{EB}=50 \text{ ohm}$  | 650                     | $I_{C}=1\Lambda, R_{EB}=50$ ohm   |
| I <sub>AC</sub> (A)        | 50        | h <sub>FE</sub> =30  | 50                      | h <sub>FE</sub> =6  |
| h <sub>FE</sub>            | 30        | V <sub>CE</sub> =2V, I <sub>C</sub> =50A, T <sub>j</sub> =1250                       | 6                       | $v_{cE} = 2V, I_{c} = 50A, T_{j} = 125^{\circ}C$                                    |
| V <sub>CE(sat)</sub> (V)   | 0.36      | $I_{C}=50A$ , $I_{B}=4A$   | 0.49                    | I <sub>C</sub> =50A, I <sub>B</sub> =10A  |
| t <sub>r</sub> (µs)        | 0.17      | V <sub>CC</sub> =300V,I <sub>C</sub> =50A<br>I <sub>B1</sub> =4A,I <sub>B2</sub> =5Λ | 0.50                    | V <sub>CC</sub> =300V,I <sub>C</sub> =50A<br>I <sub>B1</sub> =-I <sub>E2</sub> =10A |
| t <sub>stg</sub> (µs)      | 3.5       |  | 2.5                     |   |
| t <sub>f</sub> (µs)        | 0.15      |  | 0.30                    |   |