

B—3—5 A Novel Integrated Optical Bistable Device

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Optical bistable devices (OBDs) are expected as essential elements for optical information processing. Many reports have been published about OBDs. The OBDs are classified into two groups. One is achieved by using a variety of nonlinear optical materials.¹ These materials show the nonlinear dependence of refractive indices on the incident light power. To achieve the bistable condition, however, it requires very high intensity of light. The other is achieved by using a "hybrid" technique.² The light which passes through an electro-optic (EO) material is detected by photodetector, and the output voltage is applied to the electrodes on the EO material to modulate the refractive indices. The "hybrid" OBDs reported to the present, however, require an external amplifier to obtain a sufficient drive voltage.

In this paper, we report a novel integrated OBD in which the electrical feedback loop is integrated monolithically. Figure 1 shows a scheme of proposed optical bistable device in which interdigital electrode Bragg deflector and amorphous silicon photovoltaic detector are integrated on Ti-indiffused Y-cut LiNbO₃. The principle of operation is as follows. The light P_i incident on the Bragg deflector is divided into transmitted light P_t and reflected light P_r. The transmission efficiency P_t/P_i of the Bragg deflector is given by following equations.³

$$P_t/P_i = \beta \cos^2(\pi \Delta n d / \lambda_0 \cos \theta) + \alpha, \quad \Delta n = 0.5 \gamma_{33} n_e^3 E$$

Where Δn is an induced refractive index change, d a width of the Bragg deflector, λ_0 a free space wavelength, θ a Bragg angle (a function of grating pitch), γ_{33} an electro-optic coefficient, n_e an extraordinary index, and E an applied electric field. Figure 2 shows an example of calculated results which shows the dependence of P_t/P_i on the output voltage V [A], and the dependence of the V on the P_t with the P_i as a parameter [B]. As the P_i increases, the P_t moves from a to c. As the P_i exceeds 0.028 mW, the P_t jumps from c to d. Figure 3 shows the dependence of the P_t on the P_i with the voltage which gives minimum P_t/P_i as a parameter. It shows the hysteresis characteristics of bistable operation.

In the experiment, the Bragg deflector with 2 μm pitch, corresponding to

$\theta=1.04^\circ$, was fabricated on the substrate. The detector, 20 amorphous silicon photovoltaic cells connected in tandem (as shown in Figure 1), produced the maximum voltage of more than 12 V. Figure 4 shows the characteristics of P_t as a function of P_i . The differential amplification at $P_i=0.065$ mW and the bistability with hysteresis between $P_i=0.12$ mW and 0.15 mW correspond to the 1st and 2nd lobes of the P_t/P_i curve which differed from the ideal cos curve [A] shown in Figure 2.

In conclusion, a novel OBD integrating electrical feedback loop has been experimentally shown. Amorphous silicon photodetector is easily deposited on any place of the substrate, and the feasibility of the fabrication of complex OBDs will be expected.

References

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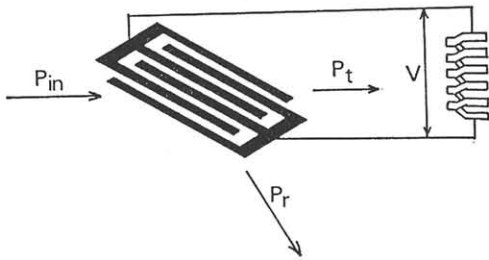


Figure 1. Schematic diagram of Integrated OBD

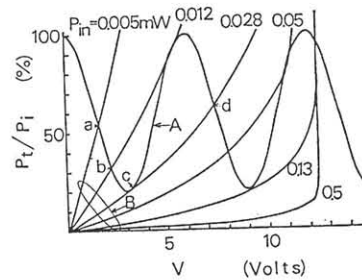


Figure 2. Dependence of P_t/P_i on the output voltage V [A] Dependence of V on P_t with P_i as a parameter.

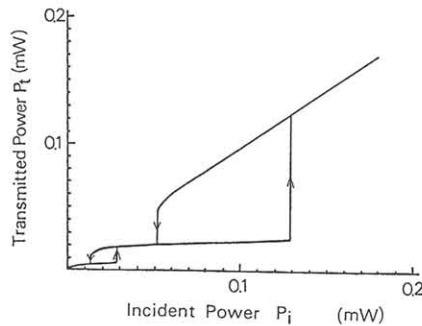


Figure 3. Hysteresis characteristics of OBD.

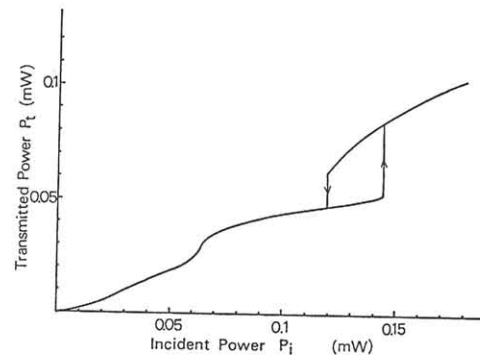


Figure 4. Experimental result.