EBX and Mass-Transport Techniques for Phase-Shifted DFB Laser

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A method for fabricating phase-shifted DFB laser is presented. The method is a combination between the use of electron beam lithography method for fabrication of corrugation with desired phase-shift and mass-transport technique for reduction of threshold current and facet reflectivity. Low threshold current and stable single mode operation at the Bragg wavelength was measured. This method is convenient since lesscomplex processes were involved.

I. Introduction.

Facing the incoming era of long wavelength optical fiber communication system, the development of the dynamic single mode (DSM) semiconductor laser¹⁾ as a light source is very important. The DSM laser can operate in single longitudinal mode under high speed modulation, various degree of injection current, and temperature variations.

The phase-shifted DFB laser,²⁻⁶⁾ that recently developed experimentally^{7,8)} in order to solve the 'two modes problem' of conventional DFB laser, is one of the promising DSM lasers. The feature of phase-shifted DFB laser is its ability to operate stably in a single longitudinal mode operation at the Bragg wavelength, which is made possible by introducing a phase shift to the corrugated structure in the middle part of cavity and by reducing reflectivity of facets.

We report here a method for fabrication of phase-shifted DFB laser. The method is a combination between the use of the electron beam lithography for obtaining corrugation with desired phaseshift and the mass-transport technique for reduction of the threshold current and as well as the effect of facet reflectivity.⁹⁾

a)



Fig.1. a)schematic diagram of phaseshifted DFB laser b)threshold gain vs deviation from Bragg wavelength

2. Device Structure.

The schematic diagram of device is shown in Fig.1a. The Bragg wavelength oscillation can be achieved, providing negligible facets reflectivity and $\Lambda/2m($ Λ = corrugation pitch, m = corrugation order) phase shift is introduced in corrugated structure⁶. This structure leads to the lowest threshold gain in Bragg wavelength while the threhold gain difference between main mode and submode be maximized(Fig.1b) and, therefore, offering stable single mode operation.

The fabricated device structure is shown in Fig. 2, consist of an active region with phase-shifted corrugated structure and mass-transported window regions connected to the ends of cavity.



Fig.2. Device structure

3. Fabrication process.

3.1. Fabrication of corrugation.

The first step in fabrication process is forming the corrugation with phase shift on n-InP substrate. Since it was rather difficult to make a phase shift to the corrugation by conventional laser beam interference method, we employed electron beam lithography method to define the corrugation. The line pitch is 4630 Å, which is corresponds to the 2nd order grating for lasing at peak photoluminescence wavelength. Since for 1 mm² scanning area the diameter of scanning spot is 625Å, for 1.5-1.6µm range GaInAsP/InP lasers that have pitches of corrugation around 4600-4700Å, 8 points is necessary to define the lines. In order to make fine pitch adjustment, an attenuator is inserted between gun deflector and control unit.¹⁰⁾ OEBR 1000 is used as electron beam resist. The patterns size are 330x100 μ m², applied voltage is 20kV and



Fig.3. SEM picture of grating profile after etching process



Fig.4. SEM picture of grating obtained by EBX method(top view)

absorption current is 10^{-10} A. Scanning speed is 5×10^4 points/sec and each pattern are drawn within 45 sec. The pattern was then developed by OEBR developer and transcribed to InP substrate by HBr+HNO₃+10H₂O etchant. After etching, the grating depth was about 1500-2000Å. Fig. 3 shows the SEM picture of grating profile after etching process. As can be seen from Fig.4, uniform and smooth grating was obtained

by EBX method.

3.2. Material growth.

After fabrication of corrugation, the 0.2µm thick n-GaInAsP buffer $(\lambda = 1.35 \mu m)$, 0.2 μm thick undoped active($\lambda = 1.55 \mu m$), p-InP clad and p-GaInAsP cap layers were successively grown on the corrugation using LPE technique. The soak and growth temperatures are 610°C and 590°C, respectively. Fig.5 shows the SEM picture of layer structure cross-section(marked part of Fig.2) after growth. The grating depth after growth is about 800-1000Å. Interesting to see that after growth, the boundary part of pattern is not perfectly buried with epitaxial layers. This fact was helpful to recognize the pattern,



Fig.5. SEM picture of layer structure after growth

which important for proceeding the next process.

3.3. Mass-transport technique for reduction of threshold current and facet reflectivity.

Mass-transport technique was recently developed to obtain stable single transverse mode and reduction of threshold current.¹¹⁾ As an alternative method instead of conventional BH structure method, the unique feature of mass-transport technique is its simplicity in forming buried structure to the active layer. In our experiment, we also employed this technique to form the anti-reflecting structure for reduction of facet reflectivity.

First, the SiO₂ mask was deposited on the wafer. Then, the conventional photolithography and etching method were used to form mesa structure. The mask used to form BH and antireflecting structure simultaneously is shown in Fig.6. The active regions consist of 7μ m wide and 300μ m long sections, which connected to 5μ m wide and 50μ m long window sections. The etchants



Fig.6, Mask pattern for BH and window region

used for forming the mesa are Brmethanol and 4HCl+H2O. By observing the etched rate in dummy sections that have the same width as window sections during undercutting process using $3H_2SO_4+H_2O+H_2O_2$, we could obtain $1-2\mu m$ active stripes in the active regions(Fig.6c) and air bridges(no active stripes) in window regions(Fig.6d). The mass-transport process were conducted in LPE furnace for 2 hours in 700°C pure H2 atmosphere, producing buried InP either in undercut parts of active region and the air bridges in window regions.

After window stripe opening, Zndiffusion and evaporation for electrode fabrication, the devices were obtained by cleaving.

About 25µm long of window region

suppresed facet reflectivity to about $1\%,^{12}$ sufficient for obtaining single mode operation.⁶⁾

4. Lasing characteristics.

As shown in Fig.7, the threshold current of 40mA and several mW/facets of light output power can be achieved. The measured light spectra is also shown. Above threshod, the stable single mode can be observed and below threshold, the



Fig.7. Measured a)I-L characteristic and b)light spectra

symmetrical spectra about the lasing wavelength were measured, indicated that lasing occured at the Bragg wavelength and therefore, showing the effect of phase-shift introduced to corrugated structure. The measured temperature dependence of lasing wavelength is 0.7A/K.

Conclusion.

We have developed EBX and masstransport technique for fabricating phase-shifted DFB laser. The low threshold and stable single longitudinal mode operation at the Bragg wavelength was measured. The method is shown very convenient since less-complex processes were involved.

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