

## High-Gain Multi-Finger AlGaIn/GaN HJFETs with 0.3- $\mu\text{m}$ Gate-Length for K- and Ka-Band Applications

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### 1. Introduction

Heterojunction field effect transistors (HJFETs) based on the AlGaIn/GaN material system are promising for high-power applications at microwave frequencies. In fact, a number of AlGaIn/GaN HJFETs have demonstrated a power density several times larger than what is possible in GaAs FETs [1]. Though these power densities have mainly been measured at frequencies lower than 10 GHz, AlGaIn/GaN HJFETs are also candidates for higher-frequency applications, such as used as K- and Ka-band power amplifiers in satellite communication systems. To date, though, only the power performance at  $f=18$  GHz of an AlGaIn/GaN HJFET with a narrow gate of  $76 \mu\text{m}$  has been reported [2].

We have fabricated AlGaIn/GaN HJFETs with a structure suitable for near-millimeter wave applications; *i.e.*, with a sub-half-micron gate-length made by electron-beam (EB) lithography, and multi-gate fingers with air-bridge interconnection. The fabricated multi-finger FETs exhibit a small-signal power gain high enough to enable K- and Ka-band applications as well as very uniform dc performance. In addition, the air-bridge interconnection prevents  $\text{SiO}_2$ -film-induced current-collapse as well as reducing the parasitic capacitance.

### 2. Device Fabrication

A cross-sectional view of the fabricated AlGaIn/GaN HJFET is shown in Fig. 1. The AlGaIn/GaN modulation-doped structure was grown on a C-plane sapphire substrate by MOVPE. Source and drain ohmic contacts were formed with Ti/Al by annealing at  $650^\circ\text{C}$  for 30 s. The contact resistance was  $2.0 \Omega\text{mm}$ . The devices were isolated by N-ion implantation with a dose of  $1 \times 10^{14} \text{ cm}^{-2}$  at energies of 20 keV and 100 keV. A T-shaped gate was patterned from two layers of PMMA/P(MMA-MAA) resists which were exposed in a single step using direct-write EB lithography. The Schottky gate was formed with Ni/Au by a lift-off method. The minimized gate length  $L_g$  was  $0.25 \mu\text{m}$ , and the minimized source-gate  $L_{sg}$  and gate-drain  $L_{gd}$  distances were  $0.5 \mu\text{m}$ , as measured by SEM.

A comb-type multi-gate configuration is usually used in microwave power FETs. In this structure, the gate bus-line must cross over the source electrode. We formed the crossover structures by air-bridge interconnection instead of by inserting an insulating  $\text{SiO}_2$  film since we found an  $\text{SiO}_2$  film on the surface induced significant current collapse in our preliminary experiments on AlGaIn/GaN HJFETs (Fig. 2). Three unit-gate widths  $W_{gu}$  of  $25 \mu\text{m}$ ,  $50 \mu\text{m}$  and  $120 \mu\text{m}$  were fabricated. The multi-finger FETs were made with an

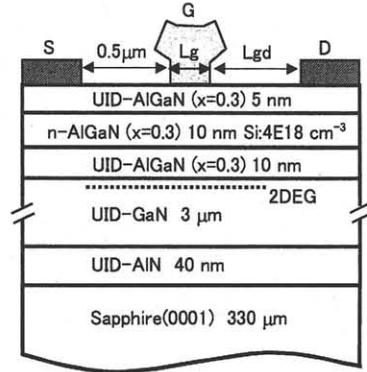


Fig. 1 Schematic cross-section of AlGaIn/GaN HJFETs,  $L_{gd}=0.5 \mu\text{m}$  for  $L_g=0.25 \mu\text{m}$ , and  $L_{gd}=0.9 \mu\text{m}$  for  $L_g=0.3 \mu\text{m}$

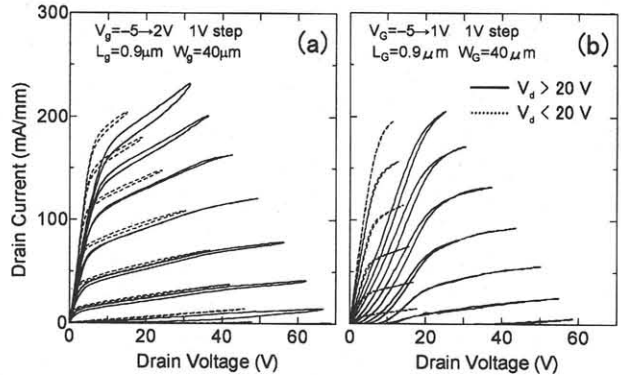


Fig. 2  $I_d$ - $V_d$  characteristics of  $0.9\text{-}\mu\text{m}$ -gate AlGaIn/GaN HJFETs (a) before, and (b) after forming a  $\text{SiO}_2$  film on the surface

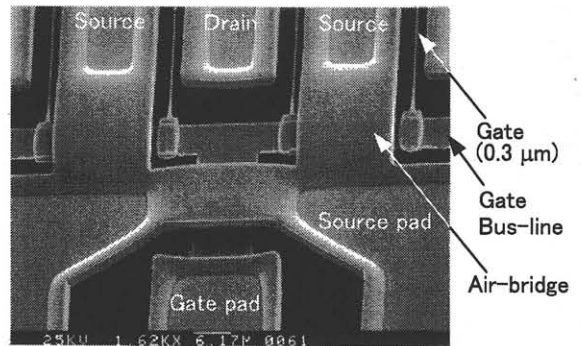


Fig. 3 SEM view of comb-type  $0.3\text{-}\mu\text{m}$  gates and an air-bridge overlay structure

offset gate structure; *i.e.*,  $L_g=0.3 \mu\text{m}$ ,  $L_{sg}=0.5 \mu\text{m}$  and  $L_{gd}=0.9 \mu\text{m}$ . An SEM image of  $0.3\text{-}\mu\text{m}$  multi-gate-fingers and air-bridge overlay structure is shown in Fig. 3.

### 3. Multi-finger FET Performance

The  $I_d$ - $V_d$  characteristics of the fabricated HJFETs with the 0.3- $\mu\text{m}$  gate-length and different gate peripheries are shown in Fig. 4. Each gate-finger operated so uniformly that the drain current was almost proportional to the total gate-width from 50  $\mu\text{m}$  to 1.2 mm (120  $\mu\text{m}$  $\times$ 10). The peak transconductance  $g_{m\text{max}}$  was 127 mS/mm. The off-state breakdown voltage was higher than 100 V when  $L_{\text{gd}}=0.9$   $\mu\text{m}$ . No significant current collapse was observed since a  $\text{SiO}_2$  film was not used on the surface.

Figure 5 shows the current gain  $|h_{21}|^2$ , the maximum available power gain  $MAG$ , and the unilateral power gain  $G_{\text{umax}}$ , calculated from on-wafer s-parameter measurements of the fabricated HJFETs with  $L_g=0.25$   $\mu\text{m}$  and  $L_{\text{sg}}=L_{\text{gd}}=0.5$   $\mu\text{m}$ . A peak cut-off frequency  $f_T$  of 40 GHz and a peak maximum oscillation frequency  $f_{\text{max}}$  of 97 GHz were obtained by extrapolating  $|h_{21}|^2$  and  $G_{\text{umax}}$  at -6 dB/octave. An intrinsic  $f_T$  of 58 GHz and an intrinsic  $f_{\text{max}}$  of 130 GHz are obtained by subtracting the measured parasitic impedance of the open- and short-pad patterns. The relatively high  $f_{\text{max}}/f_T$  ratio came from the suppression of short channel effects by using a thin (25 nm) AlGaIn layer.

The measured  $MAG$  and maximum stable power gains  $MSG$  of 0.3- $\mu\text{m}$  gate FETs with various gate peripheries are compared in Fig. 6. Two- and six-finger FETs with  $W_{\text{gu}}=50$   $\mu\text{m}$  demonstrate very similar RF performance; *i.e.*,  $MSG=13$  dB at  $f=18$  GHz and  $MAG=9.5$  dB at  $f=30$  GHz. These gains are comparable with those of 0.35- $\mu\text{m}$  gate-length AlGaAs/InGaAs PHEMTs used in K-band power applications [3]. The values of  $f_T$  and  $MSG$  increased slightly with the unit-gate width since the influence of the parasitic capacitance became weaker. When the gate periphery became large ( $W_g=120$   $\mu\text{m}$  $\times$ 10), however, the  $MSG/MAG$  break-point frequency  $f_{K=1}$  decreased due to the increased gate resistance, resulting in a degraded power gain at  $f > 10$  GHz. These findings will be useful for designing a unit-cell layout suitable for the required frequency. In addition to an inherently high breakdown voltage, AlGaIn/GaN HJFETs exhibit small-signal gains comparable with AlGaAs/InGaAs PHEMTs. Therefore, these results convince us that AlGaIn/GaN HJFETs are promising candidates for use in K- and Ka-band amplifiers and MMICs

### 4. Summary

We have successfully fabricated multi-finger AlGaIn/GaN HJFETs with 0.3- $\mu\text{m}$  gate-length using air-bridge interconnection. The fabricated multi-finger HJFETs showed a small-signal power gain high enough for K- and Ka-band applications, due to the sub-half-micron gates and the minimized parasitic capacitance, as well as uniform dc characteristics. In addition, they were free from current collapse because no  $\text{SiO}_2$  film was used on the surface. These results demonstrate the high potential of AlGaIn/GaN HJFETs for near-millimeter-wave applications.

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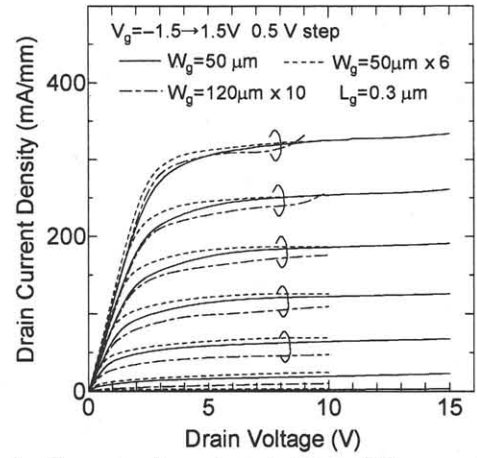


Fig. 4 Current-voltage characteristics of 0.3- $\mu\text{m}$ -gate AlGaIn/GaN HJFETs with different gate peripheries

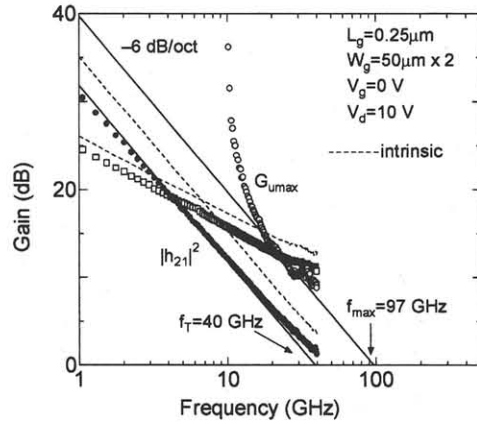


Fig. 5 Small signal gains of 0.25- $\mu\text{m}$ -gate AlGaIn/GaN HJFETs as a function of frequency

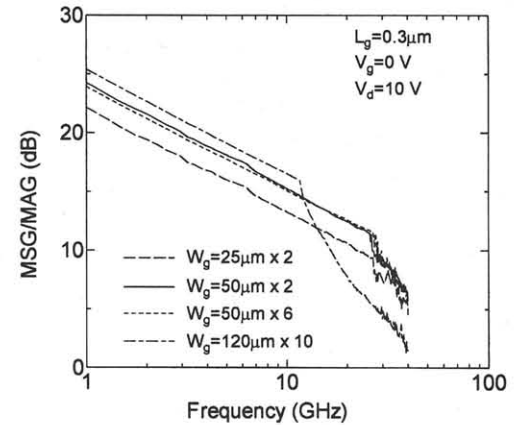


Fig. 6  $MSG/MAG$  of 0.3- $\mu\text{m}$  gate AlGaIn/GaN HJFETs with different gate peripheries

### References

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