# Acoustic Emission Characteristics of Nanocrystalline Porous Silicon Device Driven as an Ultrasonic Speaker

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### **1. Introduction**

Due to complete carrier depletion associated with strong quantum confinement effect in nanocrystalline porous silicon (nc-PS), its thermal conductivity and heat capacity per unit volume are extremely low in comparison to those of single-crystalline silicon (c-Si). The exceptionally high contrast in the thermal properties between nc-PS and c-Si induces efficient thermo-acoustic effect by which ultrasound wave is generated without any mechanical surface vibrations [1]. In this device, a dc-superimposed driving mode can effectively enhance the acoustic output amplitude, as reported previously [2]. Effects of the dc-superimposed drive are reported here in more detail for the use as a novel ultrasound generator.

# 2. Experimental

A schematic of the device structure and the experimental configuration for measurement are shown in Fig. 1. The nc-PS device is composed of a thin film heater electrode, an nc-PS laver, and a c-Si wafer. The substrates were p-type (100) c-Si wafers (80-120  $\Omega$ cm). The nc-PS layers were prepared by electrochemical anodization of a c-Si wafers in a solution of 55 % HF:ethanol=1:1 at a current density of 100 mA/cm<sup>2</sup>. The thickness of the nc-PS layer (2 µm in this case) was adjusted to a value that was considerably larger than the thermal diffusion length in the nc-PS layer at frequencies under study. After anodization, a thin tungsten film (50 nm in thickness) was deposited by RF-sputtering onto the nc-PS layer and used as a heater electrode. The heater electrode size corresponding to the ultrasonic emission area was  $5 \times 5 \text{ mm}^2$ .

The device was operated under the following two electrical input modes: a simple ac-voltage drive and a dc-superimposed ac-voltage one. The emitted sound pressure was measured as a function of the input power and voltage by using a microphone located at a distance of 10 mm from the device surface. A possible stationary temperature rise at the device surface was also monitored during operation by a radiation thermometer under the situation that the device was mounted on a heat sink with a heat resistance of 0.78 K/W.

# 3. Results and Discussion

Since the acoustic pressure generated in the nc-PS emitter is principally proportional to the amplitude of surface temperature fluctuations to be induced by Joule heating, the output pressure for a simple ac-voltage input  $V_{p-p} \sin\omega t$  is represented by  $\propto V_{p-p}^{-2} \cos 2\omega t$ , where  $V_{p-p}$  is an input voltage in peak-to-peak. When a dc-superimposed voltage  $V_{dc}+V_{p-p}\sin\omega t$  is introduced as the input, on the other hand, the major component of the output signal is given by  $\propto 2V_{dc}V_{p-p}\sin\omega t$ , where  $V_{dc}$  is an applied dc voltage.

The measured output sound pressures for the two driving modes are shown in **Fig. 2** as a function of  $V_{p-p}$ . The respective acoustic outputs exhibit the  $V_{p-p}$  dependencies along the way as expected above. It should be noted that in the dc-superimposed drive, the output frequency is the same as the input one. In addition, a stationary temperature rise is kept constant independent of  $V_{p-p}$  in contrast to the case of the ac-voltage drive. As indicated in **Fig. 3**, the linear relationship between the output and  $V_{dc}$  has been fairly confirmed in the dc-superimposed drive.

The advantageous feature in the dc-superimposed drive over the ac-voltage drive can also be seen in the input power dependence of the acoustic output, as shown in **Fig. 4**. Obviously the power efficiency is significantly enhanced in the dc-superimposed drive without affect on the temperature rise.

# 4. Conclusion

It has been shown that the dc-superimposed drive is more useful for efficient operation of the nc-PS ultrasound emitter in comparison to the conventional simple ac-voltage drive. The present result ensures the technological potential of the nc-PS ultrasound emitter for applications to functional devices such as a super tweeter and a parametric speaker.

### References

- H. Shinoda, T. Nakajima, M. Yoshiyama and N. Koshida: Nature 400 (1999) 853.
- [2] A. Kiuchi and N. Koshida: Jpn. J. Appl. Phys. 44 (2005) 2080.



**Fig. 1.** The device structure and experimental configuration. A microphone is located at a distance of 10 mm from the device surface. A stationary temperature rise at the device surface is also measured using a radiation thermometer during operation.



**Fig. 2.** Measured output sound pressures as a function of the input voltage (in peak-to-peak) under a simple ac-voltage drive mode (input frequency: 25 kHz) and a dc-superimposed drive one (input frequency: 50 kHz). Detected stationary temperature rises at the device surface under the two drive modes are also shown by the open plots.



**Fig. 3.** Measured sound pressure output and stationary temperature rise at the device surface as a function of dc-superimposed voltage  $V_{dc}$ . The input voltage Vp-p and the input frequency are 5 V and 50 kHz, respectively, in this case.



**Fig. 4.** Input power dependencies of measured output sound pressures under an ac-voltage drive mode (input frequency: 25 kHz) and a dc-superimposed drive one (input frequency: 50 kHz). In the case of dc-superimposed operation mode,  $V_{dc}$  is adjusted to  $V_{p-p}/2$ . Detected stationary temperature rises at the device surface under the two drive modes are also shown by the open plots.