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High frequency dielectric mapping using un-contact probe for dielectric materials

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1.Introduction

Nowadays, dielectric devices, such as multi-layered ceramics capacitors (MLCCs), were miniaturized and used at high frequency region. Recently, the local dipole moment behavior in miniaturized MLCCs has been reported about their core-shell structure.[1] The uneven dipole moment behavior in dielectric materials is well known, and local dipole moment behavior should be also investigated in high frequency region. The local dipole moment behaviors were difficult to be investigated from total dielectric properties. Therefore a high frequency measurement method for the local dielectric properties should be developed.

Identically, a high frequency measurement method for the local dielectric properties is desired as follows below, i) measurable local dipole moment behavior, ii) prevent resonance effect, and iii) frequency free. Therefore, un-contact probe is useful as the high frequency measurement method, however the impedance (Z) in measurement system is changed as a function of phase in input electric (E) field. In this report, we propose a measurement method for high frequency region. The reflection intensity (r) using un-contact probe was measured in high frequency, and r was successfully transformed to dielectric permittivity (ϵ_r).

2.Experimental

Figure 1 shows the measurement system and simulation model. The measurement system was, as shown in Fig.1(a), constructed from an oscillator generated by a gun diode (8.5-11GHz), phase shifter (0-360°), directional coupler, detector (diode), test-probe (0.99mm ϕ , Micro Denshi Co. Ltd.) and micro-probe (6 μ m ϕ , KEYCOM Corp.). The frequency was ranged from 8.5GHz to 11GHz. The test-probe was formed from semi-rigid coaxial cable. The test-probe was sized 8mm for length.

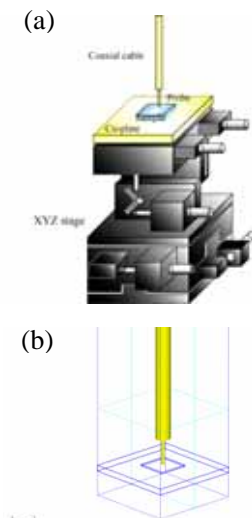


Fig.1 The measurement system (a) and simulation model for electromagnetic analysis (b).

The micro-probe was sized also 8mm, and it was attached to top of coaxial cable. The XYZ-stage was moved by d.c. servomotors (Chuo precision industrial Co.Ltd.) for setting to each axes, and they are controlled by a personal computer using GP-IB interface. The sample was selected for Cu-plate (reference, size: 40x40x2.0mm³), Al₂O₃(1000) (ALO) and SrTiO₃(100) (STO) substrates (Shinko-sha Co.Inc., size: 10x10x0.5mm³). The reflection intensity (r) was measured at room temperature as a function of distance (d) between probe and sample. In addition, the scanning for XY-plane was carried out for samples.

The electromagnetic (EM) analysis was carried out using finite differential time domain (FDTD) method using MAGNA/TDM software (CRC solutions Corp.). Figure 1(b) shows the simulation model. The size and physical quantities were input to the simulation model, and then Gaussian pulse was loaded to simulation model. The reflection coefficient (I) and Z were calculated using results of EM field distribution.

3.Results and Discussion

3.1 Reflection intensity for Cu-plate

Figure 2 shows the r intensity for Cu-plate as a function of distance between probe and Cu-plate at 9.4GHz. The r intensity showed minimum value at $d=0.2$ mm only at 9.4GHz,

and r at other frequencies was increased with decreasing d in Fig.1(a). Figure 3 shows the r intensity for ALO and STO as a function of d . The r was increased with increasing ϵ_r of sample (ALO: $\epsilon_r=10$, STO: $\epsilon_r=310$). In order to investigate r property, the EM analysis was carried out using simulation model in Fig. 1(b).

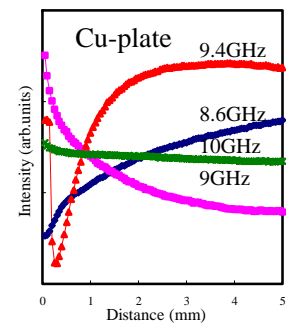


Fig.2 Reflection intensity for Cu-plate as a function of distance.

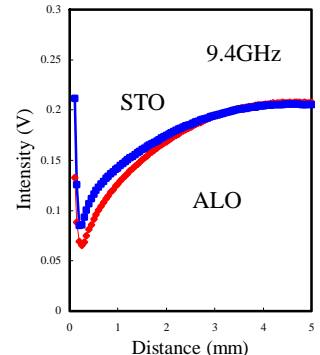


Fig.3 Reflection intensity of Al₂O₃ and SrTiO₃.

3.2 Results of electromagnetic analysis

The E field distribution of ALO ($\epsilon_r=10$) was calculated by EM analysis. The E field distributes to space and sample surface, and obtained E distribution presents a dipole antenna. From E field distribution, Γ , Z and θ of Γ were calculated. Figure 4 shows Γ as a function of d . Γ is also presents minimum value at $d=0.2\text{mm}$. The Γ and Z were calculated 0.34 and 98.7Ω at $d=0.2\text{mm}$, respectively. The relationship between Γ and Z is expressed in eq.(1)

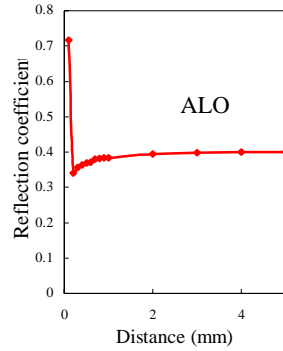


Fig.4 Reflection intensity of Al_2O_3 calculated by electromagnetic analysis.

$$\Gamma = (Z - Z_0) / (Z + Z_0), \quad (1)$$

where Z_0 is the characteristic Z defined as 50Ω . The Γ and Z at $d=0.2\text{mm}$ in Fig.4 are well accordance with eq.(1).[2]

3.3 Reflection intensity and reflection coefficient of ALO and STO

Figure 5 shows the r (Fig.3) and Γ (Fig.4) properties of ALO and STO. (The open circle is calculated value of EM analysis.) At $d=0.2\text{mm}$, Γ of ALO and STO is 0.34 and 0.36. From results in section 3.2, impedance matching was found at $d=0.2\text{mm}$. Hence, the d presents minimum r can be considered as the electrical length (l).

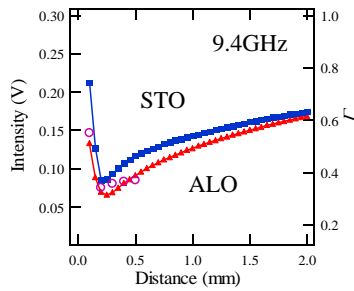


Fig.5 Plots of reflection intensities (experimental) and coefficient (analysis) of Al_2O_3 and SrTiO_3 .

3.4 Transform to dielectric permittivity

From the result in section 3.3, Z in eq.(1) indicates Z of sample ($Z = 1/j\omega C$, where C is capacitance of sample). The C of sample is $C = \epsilon_r \epsilon_0 S / d_0$, where S is effective EM wave irradiated to sample. The S was calculated from eq.(1) as $Z = Z_l$.

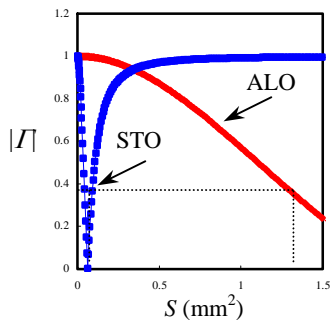


Fig.6 Reflection coefficient versus effective area.

Figure 6 shows the Γ as a function of S . The S was decided to be 1.33mm^2 (ALO) and 0.06mm^2 (STO) in Fig.6. As shown in Fig.6, S was decreased with increasing ϵ_r . From above discussion, the ϵ_r at $d=0.2\text{mm}$ was estimated using eq.(2)

$$\epsilon_r = 2|\Gamma| \sin \theta [\omega C_0 Z_0 (|\Gamma|^2 + 2|\Gamma| \cos \theta + 1)], \quad (2)$$

where $\theta=90^\circ$, $\omega=2\pi f$, $C_0=\epsilon_0 S/(0.5\text{mm})$ and $Z_0=50\Omega$. [3] Figure 7 shows the ϵ_r versus l . The ϵ_r of ALO and STO is estimated to be 8.9 and 290. The ϵ_r in Fig.7 is accordance with the ϵ_r of samples. Figure 8 shows the r mapping of ALO at 9.4GHz. The obtained mapping shows the homogeneous distribution of r reflecting ϵ_r of ALO.

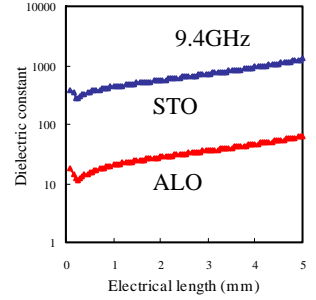


Fig.7 Dielectric permittivity of samples versus electrical length.

4. Conclusion

Using un-contact probe, the reflection intensity measurement at high frequency was carried out for dielectric materials. The reflection intensity showed the minimum value at distance of 0.2mm. The reflection intensity minimum point presented an impedance matching one. The dielectric permittivity of samples was calculated by using reflection intensity minimum point value and result of electromagnetic analysis. In addition to dielectric permittivity calculation, in-plane reflection intensity mapping was also obtained.



Fig.8 Reflection intensity mapping of $\text{Al}_2\text{O}_3/\text{Cu}$ -plate.

Acknowledgment

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Reference

- 1) H.Chazono and H.Kishi, Jpn. J. Appl. Phys. **40** (2001) 5624.
- 2) H.Kakemoto, J.Li, S-M. Num, S.Wada and T.Tsurumi: Jpn. J. Appl. Phys. **42** (2001) 6143.
- 3) S.S.Stuchly, M.A.Rzepecka, and M.F.Iskander, IEEE Trans. Instrum. Meas. **23** (1974) 56.